

# stab.routh Routh-Hurwitz criterion

There is no practical way to find the roots of a polynomial greater than degree four.<sup>7</sup> An implication of this is that we cannot practically solve (analytically) for the poles of a closed-loop transfer function with degree greater than four. Fortunately, **numerical root finders** can handle these higher-order systems with ease. However, there is a drawback to using numerical root finders to determine stability: design parameters, which show up in the coefficients of the denominator polynomial of a transfer function, must be assigned a specific value. A couple of mathematicians<sup>8</sup> in the late 19<sup>th</sup> century came up with a clever test—called the **Routh-Hurwitz stability criterion**<sup>9</sup>—for learning much about the stability of a system without computing its poles; moreover, the test yields an analytically tractable way to determine ranges over which design parameters yield stable closed-loop systems.

## An algorithm for applying the Routh-Hurwitz criterion

We consider an algorithm for this test. First, we address the “basic” algorithm and refer the reader to Nise<sup>10</sup> for the two exceptions that arise when Column 1 has a zero or when an entire row is zero. You can teach this algorithm (including the exceptions) to a computer, as [some have](#), but it is easy enough by-hand for many systems.

Let the denominator of a closed-loop transfer function, with real coefficients  $a_i$  be

$$a_0s^n + a_1s^{n-1} + \dots + a_{n-1}s + a_n,$$

where  $n$  a finite integer greater than or equal to the order of the numerator polynomial and  $a_0 > 0$  (if it is not, make it so by multiplication by  $-1$ ). Perform the following two steps.

7. For the interested reader, see [this stackexchange discussion](#).

### numerical root finders

8. Edward John Routh and Adolf Hurwitz were their names.

### Routh-Hurwitz stability criterion

9. It is noteworthy that the criterion is based on the [Routh-Hurwitz theorem](#).

10. Nise, *Control Systems Engineering, 7th Edition*.

**Table routh.1:** the general form of the Routh table. Empty cells are always zero.

	1	2	3	4	...	...
$s^n$	$a_0$	$a_2$	$a_4$	$a_6$	...	...
$s^{n-1}$	$a_1$	$a_3$	$a_5$	$a_7$	...	...
$s^{n-2}$	$b_1$	$b_2$	$b_3$	$b_4$	...	...
$s^{n-3}$	$c_1$	$c_2$	$c_3$	$c_4$	...	...
$s^{n-4}$	$d_1$	$d_2$	$d_3$	$d_4$	...	...
$\vdots$	$\vdots$	$\vdots$	$\vdots$	$\vdots$		
$s^2$	$e_1$	$e_2$				
$s^1$	$f_1$					
$s^0$	$g_1$					

First, construct a **Routh table**. The procedure is to fill in the general form of the Routh table, shown in **Table routh.1**, with the definitions:

$$\begin{aligned}
 b_1 &= -\frac{1}{a_1} \begin{vmatrix} a_0 & a_2 \\ a_1 & a_3 \end{vmatrix}, & b_2 &= -\frac{1}{a_1} \begin{vmatrix} a_0 & a_4 \\ a_1 & a_5 \end{vmatrix}, & b_3 &= -\frac{1}{a_1} \begin{vmatrix} a_0 & a_6 \\ a_1 & a_7 \end{vmatrix}, & \dots & (1) \\
 c_1 &= -\frac{1}{b_1} \begin{vmatrix} a_1 & a_3 \\ b_1 & b_2 \end{vmatrix}, & c_2 &= -\frac{1}{b_1} \begin{vmatrix} a_1 & a_5 \\ b_1 & b_3 \end{vmatrix}, & c_3 &= -\frac{1}{b_1} \begin{vmatrix} a_1 & a_7 \\ b_1 & b_4 \end{vmatrix}, & \dots & \\
 d_1 &= -\frac{1}{c_1} \begin{vmatrix} b_1 & b_2 \\ c_1 & c_2 \end{vmatrix}, & d_2 &= -\frac{1}{c_1} \begin{vmatrix} b_1 & b_3 \\ c_1 & c_3 \end{vmatrix}, & d_3 &= -\frac{1}{c_1} \begin{vmatrix} b_1 & b_4 \\ c_1 & c_4 \end{vmatrix}, & \dots & \\
 \vdots & & \vdots & & \vdots & & \\
 g_1 &= -\frac{1}{f_1} \begin{vmatrix} e_1 & e_2 \\ f_1 & 0 \end{vmatrix}, & g_2 &= -\frac{1}{f_1} \begin{vmatrix} e_1 & 0 \\ f_1 & 0 \end{vmatrix}, & g_3 &= -\frac{1}{f_1} \begin{vmatrix} 0 & 0 \\ 0 & 0 \end{vmatrix}.
 \end{aligned}$$

Note the pattern that emerges in **Equation 1**. The number of rows and potentially nonzero columns are  $n + 1$  and  $\lceil (n + 1)/2 \rceil$ . Potentially nonzero values hug Column 1. Descending rows, the number of potentially nonzero coefficients decreases.

The second step is to **interpret** the Routh table. For the basic Routh table, no poles lie on the imaginary axis (which excludes marginal stability), so interpretation is simple: *the number of sign changes in Column 1 is equal to the number of poles in the right half-plane—and all others are in the left half-plane*. Therefore, the system is strictly stable if its Routh array is of the basic type and has no sign changes in Column 1.

**basic Routh table interpretation**

**Example stab.routh-1**

Given the closed-loop transfer function

$$\frac{s + 7}{s^3 + 3s^2 + s + k} \tag{2}$$

where  $k$  is a design parameter, using the Routh-Hurwitz criterion, find the range of  $k$  for which the closed-loop system is stable.

- Let's build the Routh table in **Table routh.2**.
- The lower entries were computed from

**re: Basic Routh table with an unknown parameter**

Equation 1 (n.b. we knew  $b_2 = 0$ , but compute it for demonstrative purposes) as follows:

$$b_1 = -\frac{1}{a_1} \begin{vmatrix} a_0 & a_2 \\ a_1 & a_3 \end{vmatrix} = -\frac{1}{a_1} \begin{vmatrix} - & - \\ - & - \end{vmatrix} = \underline{\hspace{2cm}},$$

$$b_2 = -\frac{1}{a_1} \begin{vmatrix} a_0 & a_4 \\ a_1 & a_5 \end{vmatrix} = -\frac{1}{a_1} \begin{vmatrix} - & - \\ - & - \end{vmatrix} = \underline{\hspace{1cm}}, \text{ and}$$

$$c_1 = -\frac{1}{b_1} \begin{vmatrix} a_1 & a_3 \\ b_1 & b_2 \end{vmatrix} = -\frac{1}{b_1} \begin{vmatrix} - & - \\ - & - \end{vmatrix} = \underline{\hspace{1cm}}.$$

**Table routh.2:** Routh table for Example stab.routh-1.

	1	2	3
$s^3$	<u>  </u>	<u>  </u>	0
$s^2$	<u>  </u>	<u>  </u>	0
$s^1$	<u>  </u>	<u>  </u>	0
$s^0$	<u>  </u>	0	0

→

	1	2	3
$s^3$	<u>  </u>	<u>  </u>	0
$s^2$	<u>  </u>	<u>  </u>	0
$s^1$	<u>  </u>	<u>  </u>	0
$s^0$	<u>  </u>	0	0

Now we must interpret the result. Since the first two entries in Column 1 are positive, the last two must be in order for the system stability. The conditions are:

$$\underline{\hspace{2cm}} > 0 \Rightarrow \underline{\hspace{1cm}} \text{ and}$$

$$k > \underline{\hspace{1cm}}.$$

Therefore, the range for stability is           .  
 Expressed as an interval,  $k \in \underline{\hspace{2cm}}$ .