

## Lecture 03.03 First-order measurement systems

First order measurement systems have input-output differential equations of the form

$$\tau \frac{dy}{dt} + y = b_1 \frac{du}{dt} + b_0 u \quad (03.10)$$

with  $\tau \in \mathbb{R}$  called the *time constant* of the system. Measurement systems with a single energy storage element—such as those with electrical or thermal capacitance—can be modeled with first-order systems. time constant

### 03.03.1 Step response

Commonly, a scaling of the *unit step function*  $u_s(t)$ , which is 0 for  $t < 0$  and 1 for  $t \geq 0$ , can be considered the input to this and other measurement systems (e.g. whenever the input is changed suddenly,  $u_s$  is a good approximation). If we consider the common situation that  $b_1 = 0$  and  $u(t) = Ku_s(t)$  for some  $K \in \mathbb{R}$ , the solution to Equation 03.10 is unit step function

If we assume the steady-state solution is the proper measurement value, the transient response is *error*. Considering it never reaches zero in finite

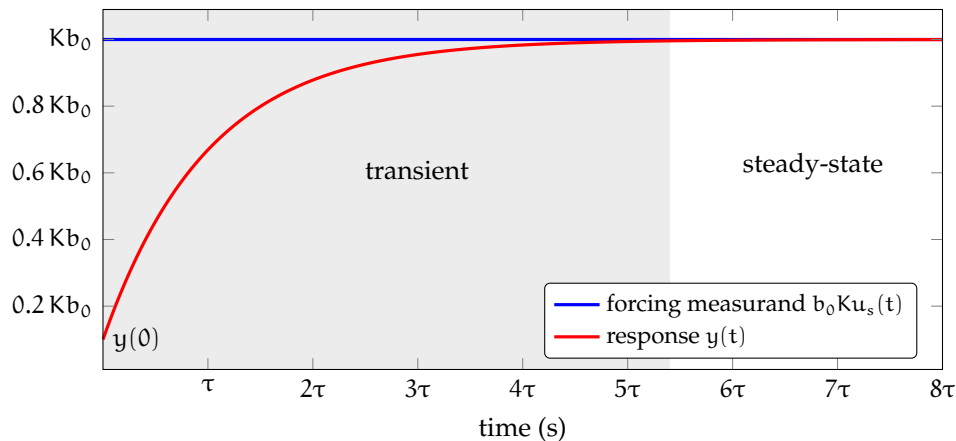


Figure 03.4: (step) response  $y(t)$  of a first order system with input  $u(t) = Ku_s(t)$  and  $b_1 = 0$ .

time, this is a bummer ☹. However, it does decay exponentially, so in  $5\tau$ , the transient response is less than 1 % of difference between  $y(0)$  and steady-state. A plot of the step response is shown in [Figure 03.4](#).

### 03.03.2 Sinusoidal response

Another common input to first-order measurement systems modeled by [Equation 03.10](#) is the sinusoid  $u(t) = A \sin \omega t$ . For  $b_1 = 0$ , the solution is

where  $\kappa$  can be found from the initial condition  $y(0)$  to be

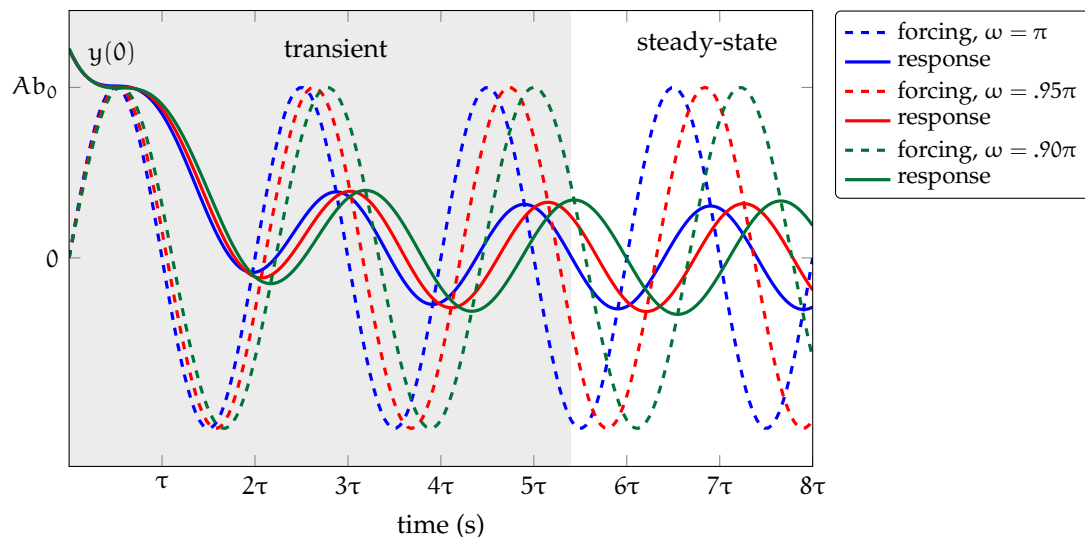
$$\kappa = y(0) + \frac{b_0 A}{\sqrt{1 + (\omega\tau)^2}} \sin(\arctan(\omega\tau)). \quad (03.11)$$

[Figure 03.5](#) shows responses of a first-order measurement system to sinusoidal inputs (measurands) at different frequencies  $\omega$ . Note the transient response decays with the same rate  $\tau$  no matter the input frequency. However, there are two differences in the steady-state responses: the amplitude and phase. In fact, the steady-state amplitude and phase of an output compared to an input present a form of *error* in the measurement. Ideally, the ratio of the output and input is unity; however, for positive  $\omega$ , this is never quite the case. We define this ratio, called the *magnitude ratio*  $M(\omega)$ , to be the steady-state output amplitude over the forcing amplitude. For first-order systems,

**magnitude ratio**  
 $M(\omega)$

**dynamic error** A metric for the nearness of  $M(\omega)$  to unity is called the *dynamic error*  $\delta(\omega)$ , given by

Ideally,  $\delta(\omega) = 0$ , but as we can see from the expression for  $M(\omega)$ , this is only ever approximately true for nonzero  $\tau$  and  $\omega$ . However, it is small when the product  $\omega\tau$  is small. So, in order to minimize dynamic



**Figure 03.5:** response  $y(t)$  of a first order system with input  $u(t) = A \sin \omega t$  and  $b_1 = 0$  for three values of  $\omega$ . The forcing function (measurand) is  $b_0 A \sin \omega t$ .

error for the measurement of a sinusoid at a given frequency, we must strive to minimize the time constant  $\tau$ . It is common to call “good enough”  $M(\omega) \geq .707$ .

Similarly, the phase difference of the output relative to the input is ideally zero. Therefore, the phase shift  $\phi(\omega)$  is another type of error and, for first-order systems, is given by

This corresponds to a *time-delay*  $\beta_1(\omega)$  in the measurement:

**time-delay**  $\beta_1(\omega)$

Clearly, we want to minimize  $\phi(\omega)$  and  $\beta_1(\omega)$ . Typically, this is achieved by minimizing  $\tau$ , which corresponds to the minimization of  $\tau$  for the minimization of the dynamic error.

Note that the steady-state response of the measurement system to sinusoidal inputs is characterized by  $M(\omega)$  and  $\phi(\omega)$ . In fact, a crucial identify will be observed here:

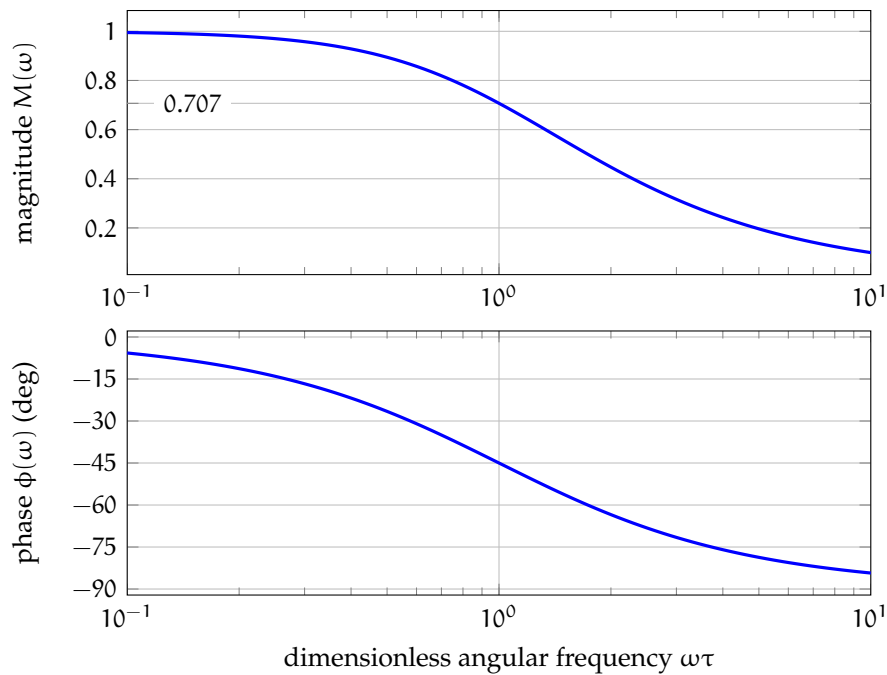


Figure 03.6: the magnitude ratio and phase.

*the magnitude ratio  $M(\omega)$  and phase  $\phi(\omega)$  are equal to the magnitude  $|H(j\omega)|$  and phase  $\angle H(j\omega)$  of the frequency response function  $H(j\omega)$ .*

This is recognized as being the complex amplitude of the output over the input, which are plotted in [Figure 03.6](#).