08.4 thermoflu.dam State-space model of a hydroelectric dam

1 Consider the microhydroelectric dam of Example 08.3 thermoflu.flutrans-1. We derived the linear graph of Fig. dam.1. In this lecture, we will derive a state-space model for the system—specifically, a state equation.

Normal tree, order, and variables

2 Now, we define a **normal tree** by overlaying it on the system graph in Fig. dam.1. There are six independent energy storage elements, making it a sixth-order (n = 6) system. We define the state vector to be

$$\mathbf{x} = \begin{bmatrix} \mathsf{P}_{\mathsf{C}_1} & \mathsf{P}_{\mathsf{C}_2} & \mathsf{Q}_{\mathsf{L}_1} & \Omega_{\mathsf{J}} & \mathfrak{i}_{\mathsf{L}_2} & \nu_{\mathsf{C}_3} \end{bmatrix}^\top.$$
(1)

The input vector is defined as $\mathbf{u} = \begin{bmatrix} Q_s & P_{s1} & P_{s2} \end{bmatrix}^\top$.

Elemental equations

3 Yet to be encountered is a turbine's transduction. A simple model is that the torque T_2 is proportional to the flowrate Q_1 , which are both



Figure dam.1: a linear graph for a microhydroelectric dam.

through-variables, making it a transformer, so

$$T_2 = -\alpha Q_1$$
 and $\Omega_2 = \frac{1}{\alpha} P_1$, (2)

where α is the **transformer ratio**.

4 The other elemental equations have been previously encountered and are listed, below.

el.	elemental eq.	el.	elemental eq. el.		elemental eq.	
C ₁	$\frac{\mathrm{d} P_{C_1}}{\mathrm{d} t} = \frac{1}{C_1} Q_{C_1}$	C ₃	$\frac{\mathrm{d}v_{\mathrm{C}_3}}{\mathrm{d}t} = \frac{1}{\mathrm{C}_3} \mathfrak{i}_{\mathrm{C}_3}$	В	$\Omega_{\rm B} = \frac{1}{\rm B} T_{\rm B}$	
C ₂	$\frac{\mathrm{d} P_{C_2}}{\mathrm{d} t} = \frac{1}{C_2} Q_{C_2}$	R_1	$P_{R_1} = Q_{R_1}R_1$	3	$i_4 = \frac{-1}{k_m} T_3$	
L ₁	$\frac{dQ_{L_1}}{dt} = \frac{1}{L_1}P_{L_1}$	R_2	$P_{R_2} = Q_{R_2}R_2$	4	$\nu_4=k_m\Omega_3$	
J	$\frac{d\Omega_J}{dt} = \frac{1}{J}T_J$	1	$T_2 = -\alpha Q_1$	R ₃	$\nu_{R_3}=i_{R_3}R_3$	
L ₂	$\frac{\mathrm{di}_{\mathrm{L}_2}}{\mathrm{dt}} = \frac{1}{\mathrm{L}_2} \nu_{\mathrm{L}_2}$	2	$\Omega_2 = \frac{1}{\alpha} P_1$	R_4	$\mathfrak{i}_{R_4}=\frac{1}{R_4}\nu_{R_4}$	

Continuity and compatibility equations

5 Continuity and compatibility equations can be found in the usual way—by drawing contours and temporarily creating loops by including links in the normal tree. We proceed by drawing a table of all elements and writing a continuity equation for each branch of the normal tree and a compatibility equation for each link.

el.	eq.	el.	eq.	el.	eq.
C ₁	$Q_{C_1} = Q_s - Q_{L_1}$	C ₃	$\mathfrak{i}_{C_3}=\mathfrak{i}_{L_2}-\mathfrak{i}_{R_4}$	В	$\Omega_B=\Omega_J$
C ₂	$Q_{C_2} = Q_{L_1}$	R_1	$Q_{R_1} = Q_{L_1}$	3	$\Omega_3=\Omega_J$
L ₁	$P_{L_1} = -P_{R_1} + P_{C_1} - P_{C_2} +$	R_2	$Q_{R_2} = Q_{L_1}$	4	$\mathfrak{i}_4=-\mathfrak{i}_{L_2}$
	$-P_{R_2} + P_{s2} - P_1 + P_{s1}$	1	$Q_1 = Q_{L_1}$	R ₃	$\mathfrak{i}_{R_3}=\mathfrak{i}_{L_2}$
J	$T_J = -T_2 - T_B - T_3$	2	$\Omega_2 = \Omega_J$	R_4	$\nu_{R_4} = \nu_{C_3}$
L_2	$\nu_{L_2} = -\nu_{R_3} + \nu_4 - \nu_{C_3}$				

State equation

6 The system of equations composed of the elemental, continuity, and compatibility equations can be reduced to the state equation. There is a substantial amount of algebra required to eliminate those variables that are neither state nor input variables. Therefore, we use the Mathematica package *StateMint* (Devine **and** Picone, 2018). The resulting system model is:

$$\begin{aligned} \frac{d\mathbf{x}}{d\mathbf{t}} &= A\mathbf{x} + B\mathbf{u}, \\ A &= \begin{bmatrix} 0 & 0 & -1/C_1 & 0 & 0 & 0 \\ 0 & 0 & 1/C_2 & 0 & 0 & 0 \\ 1/L_1 & -1/L_1 & -(R_1 + R_2)/L_1 & -\alpha/L_1 & 0 & 0 \\ 0 & 0 & \alpha/J & -B/J & -k_m/J & 0 \\ 0 & 0 & 0 & k_m/L_2 & -R_3/L_2 & -1/L_2 \\ 0 & 0 & 0 & 0 & 1/C_3 & -1/(R_4C_3) \end{bmatrix}, \\ B &= \begin{bmatrix} 1/C_1 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 1/L_1 & 1/L_1 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix}. \end{aligned}$$

7 The rub is estimating all these parameters.

STATE-SPACE MODEL OF A HYDROELECTRIC DAM

8 The Mathematica notebook used above can be found in the source repository for this text.